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(56) Documents Cited

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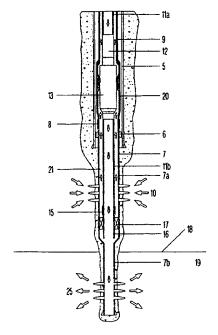
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Field of Search UK CL (Edition T) E1F FLM FMU INT CL7 E21B 43/12 43/20 **EPODOC. WPI, JAPIO**

(54) Abstract Title Downhole pump driven by injection water

(57) A method of enhancing hydrocarbon production involves pumping injection water down a wellbore to drive a downhole pump assembly (13) and using the pump assembly (13) to increase the production rate of hydrocarbons from the well. The injection water, after driving the pump assembly (13), exits through outlets (25) below a packer (17) and enters the injection zone (19) thereby driving hydrocarbons into the pump assembly (13) initially through inlets (10). The pump assembly (13) includes a turbine unit (12) driven by the movement of the injection water over turbine blades (32, fig 2).



BEST AVAILABLE COPY A Fig. 1

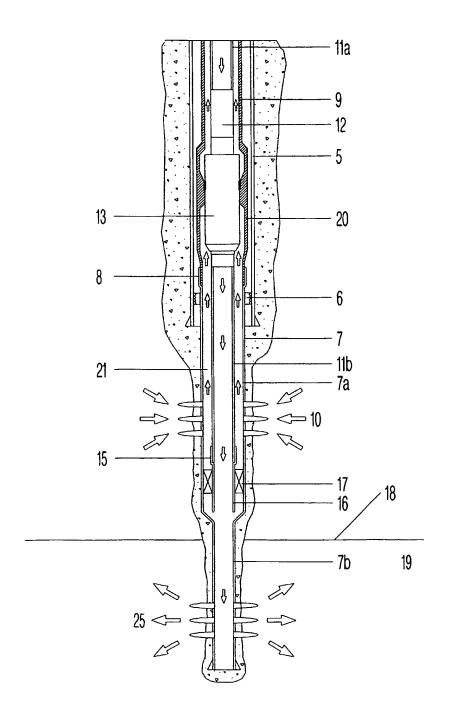


Fig. 1

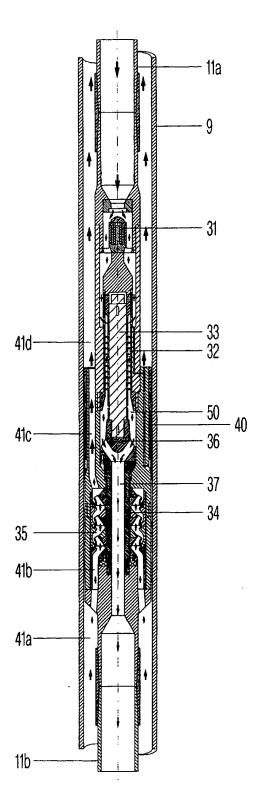
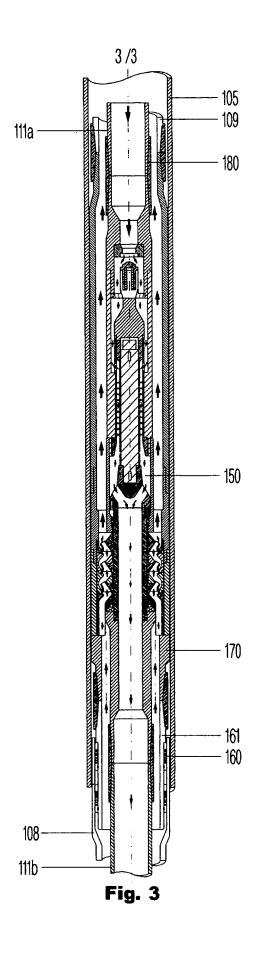


Fig. 2



1 "DOWNHOLE PUMP" 2 The present invention relates to a pump, and 3 particularly one to be installed downhole for 4 recovery of hydrocarbon fluids from drilled wells, 5 and for the injection of fluids such as water into 6 7 such wells in order to stimulate the production of fluid hydrocarbons therefrom. 8 9 Oilfield reservoirs generally consist of a layer of 10 hydrocarbon fluids such as oil which lies on top of 11 12 a denser layer of water called the aquifer. pressure wells or wells which have been produced for 13 a number of years and which no longer have 14 sufficient natural pressure to allow unaided flow of 15 hydrocarbons from the reservoir payzone to surface, 16 it is conventionally known to inject water into the 17 underlying aquifer in order to maintain or increase 18 the pressure in the reservoir and to enhance the 19 20 flow of hydrocarbon fluids into a wellbore. 21 22 According to the present invention there is provided 23 a pump for drawing a first fluid from a first end of the pump to a second end, the pump being powered by 24 the flow of a drive fluid from the second end to the 25 first, wherein the first fluid and the drive fluid 26 flow through separate conduits, one of the conduits 27

being located within the other.

29

1	The said one conduit is preferably entirely			
2	contained within the said other conduit.			
3				
4	In the pump of the invention, the drive fluid			
5	preferably goes through a first conduit, and the			
6	produced first fluid goes through the other in the			
7	opposite direction. The pump of the invention			
8	therefore avoids crossover of drive and produced			
9	fluids in the body of the pump. Certain embodiments			
10	can also minimise the complexity of downhole			
11	completion.			
12				
13	In a preferred embodiment of the invention, the			
14	drive fluid passes down an inner conduit, and the			
15	produced fluid passes up the annulus between the			
16	inner conduit and an outer tube. The blades of a			
17	turbine are preferably disposed in the path of the			
18	inner conduit and the turbine preferably provides			
19	power to a shaft which powers a pump driving the			
20	produced fluids up through the outer annulus.			
21	However, the drive fluid could equally pass through			
22	the outer annulus, and the production fluid could			
23	pass through the inner conduit. The pump in the			
24	outer annulus can be a centrifugal pump.			
25				
26	An embodiment of the invention will now be described			
27	by way of example and with reference to the			
28	accompanying drawings in which;			
29	Fig. 1 shows a schematic diagram of a pump of			
30	the present invention;			
31	Fig. 2 shows a sectional view of a pump of			
32	another embodiment;			

Fig. 3 shows a sectional view of a third 1 embodiment of a pump according to the 2 invention. 3 4 Referring now to the drawings, the well schematic 5 shown in Fig. 1 comprises a borehole lined with 6 casing 5 which is cemented in place in the borehole 7 in a conventional manner. A tapered liner 7, of 8 which 7a and 7b are the upper and lower sections, is 9 hung off from casing 5 by a liner hanger 6, is 10 cemented in situ and perforated at 10 in a reservoir 11 payzone allowing ingress of hydrocarbon fluids, and 12 is additionally perforated at its furthest extremity 13 25 to allow injection of water or other liqueous 14 The liner 7 terminates fluids into an aquifer 19. 15 at its upper end in a polished bore receptacle 8, in 16 which is received the lower end of a tieback tubing 17 string 9 which includes a dedicated sealing/locking 18 element 20, known in the industry as a nipple. 19 liner 7, nipple 20 and tieback tubing 9 provide an 20 outer string in which is disposed tubing 11a, a 21 turbine sub 12, a pump body 13 located in the nipple 22 20 and injection tubing 11b which is received in the 23 polished-bore receptacle 15 of a packer shoe 16 24 sealed by packer 17 to the cemented liner at the 25 lower end of section 7a between the perforations 10 26 and 25. Use of PBRs facilitates installation and 27 retrieval of injection tubing for maintenance etc. 28 29 The bore of the turbine sub 12, pump body 13, the 30 injection string of 11a and 11b, packer shoe 16 and 31 section 7b of liner 7 provide an inner injection 32

4

conduit located within the outer annular conduit. 1 The outer wall of the outer flow conduit comprises 2 the upper section 7a of liner 7, the outer wall of 3 the pump body 13 sealed against nipple 20 and 4 tieback tubing 9. The inner injection string is 5 located wholly within the bore of the outer string, 6 and is provided for the injection of aqueous fluid 7 such as water to the perforations 12 located in the 8 9 aquifer 19 below the oil/water interface 18 and horizontally distant from the production 10 perforations 10 so as to reduce the propensity to 11 coning. The outlet of the inner injection string is 12 located below the packers 17 thus preventing leakage 13 of water from the injection string back up the 14 15 annulus. 16 The outer wall of the annular conduit comprising the 17 cemented liner 7 and tieback tubing 9 including 18 nipple 20 directs produced fluids entering the 19 annulus 21 through perforations 10 up said annulus 20 21, through the pump body 13 and thence to surface. 21 Injection of water through the inner injection 22 string and lower perforations 25 below the oil water 23 interface 18 maintains the pressure of hydrocarbon 24 fluids entering the outer recovery string through 25 upper perforations 10 where the reservoir and 26 aquifer are in contact, and maximises recovery of 27 produced fluids from the outer annulus. 28 29 In the embodiment shown in Fig. 2, the bore of a 30 31 tieback tubing string 9 houses a single inner string of tubulars 11a and 11b for injection of fluids and 32

the annulus is provided between the inner string and 1 the tieback tubing string 9. It is noted that there 2 is no nipple in the tieback tubing string 9. 3 4 5 Tubing 11a is attached to the pump assembly in which is established a check valve sub-assembly 31. 6 7 Opening of the check valve 31 allows flow of injected fluid through to a turbine assembly in 8 which the flow of fluid is directed into the path of 9 a number of turbine blade stages 32. Flow of fluid 10 across the blades 32 causes rotation of the solid 11 shaft 33, which drives a pump shaft 34 on which are 12 mounted impeller stages 35. The respective shafts 13 are mechanically connected by flow coupling 36, said 14 flow coupling also providing passage for fluids 15 leaving the turbine stage through to the pump shaft 16 34 which is hollow. The flow coupling is an 17 important preferred feature of the invention as it 18 can simultaneously entrain the pump shaft 34 from 19 the turbine shaft 33, and ensures continuity of flow 20 from the turbine exhaust chamber 50 through the bore 21 22 37 of pump shaft 34. The flow holes through the flow coupling would preferably be shaped in the 23 manner of an impeller. Fluids leaving the turbine 24 25 blades 32 are directed into the bore 37 of the pump 26 shaft 34, said bore being in flow connection with 27 the lower tubing string 11b leading to a lower injection point into the aquifer(see Fig. 1). 28 29 The tieback string 9 is preferably landed in the 30 Xmas tree by a hanger at its upper extremity, and is 31 set in the polished bore receptacle of a tapered 32

liner at its lower extremity. A practical 1 alternative to the polished bore receptacle is use 2 of a packer. It is to the bore of string 9 that the 3 pump assembly preferably seals. The method of Fig. 4 5 1 uses an external seal, typically in the form of chevron packing, set in a dedicated receptacle of a 6 7 nipple type readily available to the industry. 8 preferred embodiment of Fig. 2 is of a pressureactivated external packer and slip system made 9 integral with, or attached to, the pump assembly. 10 The pump assembly is shown locked and sealed to the 11 tieback string 9 by a slips/seal packer. The pump 12 provides an annular flow path for produced fluids in 13 complete isolation from the injection fluids. 14 Produced fluids passing up the production annulus 15 41a enter the pump at 41b, are directed into the 16 pump impellers 35 and flow thence to surface through 17 pump exit 41c and upper annulus 41d. 18 19 The slips/seal packer assembly 40 is a standard item 20 in the industry and may be set mechanically or 21 hydraulically. The advantage in providing a packer 22 40 is that the pump can be set at any desired depth 23 within in the tieback tubing string 9. The 24 25 embodiment of Fig. 2 allows the drive fluid pressure 26 to be used to set the packer 40 although 'hot lines'- small bore tubing - may be run to the packer 27

from surface to provide setting and unsetting

2930

pressures.

28

1 The modified embodiment of the invention as shown in

- 2 Fig. 3 has many similar components and will be
- 3 referred to for ease of reference using the same
- 4 numbering system but with 100 added where required
- 5 by context. Inside the body of the pump, the
- 6 mechanical components function in essentially the
- 7 same manner as those featured in Fig. 2 and shall
- 8 only be described by exception. The principal
- 9 differences are the configurations of the tubular
- 10 and sealing elements. The size of the pump is
- limited by the internal diameter of the outer
- 12 tubular within which the pump assembly and its
- associated tubulars and seals must be run and set. A
- 14 pump assembly attached at its upper end to a tieback
- tubing string 109 is installed within a cemented
- 16 casing string 105, the tieback tubing string being
- 17 hung at the wellhead. The lower end of the pump
- 18 assembly has chevron seal elements 160 carried on a
- 19 spacer string 161, the length of the spacer string
- 20 being determined by operational requirements. For
- 21 brevity, spacer string 161 is shown as a single
- item. The chevron seals set the polished-bore
- 23 receptacle 108 which is sited at the top of the
- liner not shown but corresponds to item 7 of Fig.
- 25 1. An alternative method of achieving the lower seal
- for the pump is to use a packer to replace the PBR.
- 27 Tubular 111b, which is attached to the inner
- connection of lower body 170 of the pump, extends to
- 29 an inner PBR not shown but corresponds to item 15
- of Fig. 1. After the pump assembly has been
- installed in the well, tubing 111a is run from the
- 32 wellhead and attached the pump assembly's upper,

inner connection by a lock/seal system of which many 1 are available within the industry. It is seen on 2 Fig. 3 that the flow system is essentially the same 3 as that of Figs 1 and 2 but the size of the pump, 4 5 where the same tubular program is used on all embodiments, is significantly increased owing to the 6 7 limiting size being that of the casing 5 or 105 as referred to in Figs 1 and 3 respectively. 8 9 10 11 From this present embodiment it will be evident that 12 modifications could be made to the basic system which enhance its installation and operation under 13 various circumstances. Due to the flow coupling 14 15 having a possible castellated mating form to the pump shaft 34 then the turbine unit could be 16 separately installable/retrievable/replaceable by 17 wireline or coiled tubing to suit the pump duty as 18 downhole conditions vary with time. 19 20 21 Tubular goods sizes for drilling and completion of 22 oil wells vary for different geographical locations 23 and it should be noted that any sizes shown or cited 24 herein are typically used in the North Sea and 25 should not be construed in any limiting sense. 26 The assemblies of Figs. 1 to 3 can be located at any 27 desired depth in the well within casing string 5 28 29 which determines the maximum pump diameter. embodiments provide an outer annulus for recovery of 30 produced fluids and an inner bore for injection of a 31 32 drive fluid to power the turbines and also for

injection of fluid into the aquifer to increase 1 recovery of produced fluids from the payzone of a 2 formation. The drive fluid exhausts through the pump 3 into a targeted injection zone within the aquifer. 4 5 6 It is also possible that very high pressure fluids 7 from a deep-set abnormally pressured reservoir would provide the drive fluid to a turbine thus providing 8 9 power to a pump to drive a pump for a lower pressure reservoir sited some distance above the former. 10 This system would act as a pressure exchanger with 11 12 both fluids being produced to surface. 13 Seals, although depicted and described as chevron 14 types, can be of any desired type typically employed 15 in the industry. 16 17 It should be noted that for clarity no details of 18 shaft bearings have been shown in the drawings. 19 However, pump shaft design and bearings therefor are 20 well established and known to those in the art. 21 22 It is an especially preferred embodiment of the 23 invention to provide a seal system such as a packer 24 on a portion of the inner string so as to facilitate 25 the sealing of the inner string or a chosen location 26 27 within the outer string. 28 In certain cases, the origin of the produced fluids 29 may be multilateral branches drilled through and out 30 of the main well bore rather than perforations in 31 32 the tie back tubing.

It is anticipated that for fractured or segmented reservoirs and aquifers, the injected and produced fluids would not necessarily enter into or originate from the aquifer and reservoir of a given oil-water contact. Geological factors could dictate that the injection fluid would preferably target the aquifer beneath a neighbouring reservoir separated from that of the well by an isolating fracture.

1 CLAIMS

- 3 1. A method and apparatus for enhanced, combined
- 4 hydrocarbon production and water injection
- 5 operations in a single well wherein the method
- 6 comprises:
- 7 pumping injection water down the well to drive a
- 8 hydraulic turbine unit within a downhole pump
- 9 assembly;
- 10 utilising the pump unit to increase the
- 11 production rate of hydrocarbons from the well;
- ensuring passage of the injection water directly
- through the pump unit on exhausting from the
- turbine en route to the injection zone;
- 15 2. The apparatus of claim 1 comprising:
- an inner tubing string running from the tubing
- hanger set in the Christmas tree at the wellhead
- 18 to the downhole liner;
- 19 an outer tubing string running from the tubing
- 20 hanger set in the Christmas tree at the wellhead
- 21 to the downhole liner;
- 22 a pump assembly provided by appropriate threaded
- 23 connections as part of the inner tubing string.
- 24 3. The pump assembly of claims 1 and 2
- characterised, in combination, by:
- 26 a packoff and slips module;
- 27 a hydraulic rotary turbine mounted on and
- 28 assembled to a solid shaft;
- a hydraulic rotary pump of which the constituent
- 30 impeller stages are mounted on and assembled to a
- 31 hollow shaft;

- 1 a flow coupling linking the solid shaft of the
- 2 turbine to the hollow shaft of the pump;
- 3 a check valve set in the assembly above the
- 4 turbine unit.
- 5 4. The flow coupling of claim 3 which provides a
- 6 mechanical link from the solid shaft of the
- 7 turbine unit to the hollow shaft of the pump unit
- 8 and further permits passage of the fluid
- 9 exhausting from the turbine unit through to said
- 10 hollow shaft of the pump unit.
- 11 5. The hollow shaft of any preceding claims to which
- 12 the impeller elements of the pump are fixed and
- through which shaft the injection fluid passes to
- 14 the attached injection tubing.
- 15 6. The packoff and slips module of claim 3 which
- 16 seals and locks against the bore of the outer
- tubing string.
- 18 7. The inner tubing string of claim 2 which runs
- 19 from a tubing hanger at the wellhead to an
- 20 injection packer set within the downhole liner at
- a position below the production flow entry
 point(s) to the well and of which take
- point(s) to the well, and of which tubing string the pump assembly is an element set at a depth
- 24 appropriate to reservoir performance
- 25 characteristics.
- 26 8. The method of any preceding claims whereby
- 27 hydrocarbons emanating from the production zone
- of the well and thus being present in the lower
- 29 annulus formed by the inner and outer tubing
- 30 strings enter the pump unit at the local pressure
- and pass through the impeller stages to be
- 32 discharged from the pump unit at an elevated

pressure into the upper annulus with the packoff 1 ensuring separation of the high and low pressure 2 3 fluids across the pump. 9. The apparatus of claim 2 wherein the 4 assembly is provided as part of the outer tubing 5 6 string. 7 10. The apparatus of claims 2 and 9 wherein the lower inner tubing string runs from the pump assembly 8 to the injection packer. 9 11. The apparatus of claims 2, 9 and 10 wherein the 10 upper inner tubing string is a separate item run 11 from the wellhead to the pump assembly subsequent 12 to the installation downhole of the outer tubing 13 14 string of claim 9. 15

Amendments to the claims have been filed as follows

- 3 1. A method for enhanced, combined hydrocarbon
- 4 production and water injection operations in a
- 5 single well wherein the method comprises:
- 6 pumping injection water down the well to drive a
- 7 hydraulic turbine unit within a downhole pump
- 8 assembly;
- 9 utilising the pump unit to increase the
- 10 production rate of hydrocarbons from the well;
- ensuring passage of the injection water directly
- 12 through the pump unit on exhausting from the
- 13 turbine en route to the injection zone;
- 14 2. An apparatus to ensure the good operation of the
- 15 method of claim 1 comprising:
- an inner tubing string running from the tubing
- hanger set in the Christmas tree at the wellhead
- to the downhole liner:
- 19 an outer tubing string running from the tubing
- 20 hanger set in the Christmas tree at the wellhead
- 21 to the downhole liner;
- a pump assembly provided by appropriate threaded
- 23 connections as part of the inner tubing string.
- 24 3. The pump assembly of claim 2 further
- characterised, in combination, by:
- 26 a packoff and slips module;
- 27 a hydraulic rotary turbine mounted on and
- assembled to a solid shaft;
- a hydraulic rotary pump of which the constituent
- 30 impeller stages are mounted on and assembled to a
- 31 hollow shaft;

- a flow coupling linking the solid shaft of the
- 2 turbine to the hollow shaft of the pump;
- 3 a check valve set in the assembly above the
- 4 turbine unit.
- 5 4. The flow coupling of claim 3 which provides a
- 6 mechanical link from the solid shaft of the
- 7 turbine unit to the hollow shaft of the pump unit
- 8 and further permits passage of the fluid
- 9 exhausting from the turbine unit through to said
- 10 hollow shaft of the pump unit.
- 11 5. The hollow shaft of any preceding claims to which
- the impeller elements of the pump are fixed and
- 13 through which shaft the injection fluid passes to
- 14 the attached injection tubing.
- 15 6. The packoff and slips module of claim 3 which
- seals and locks against the bore of the outer
- 17 tubing string.
- 18 7. The inner tubing string of claim 2 which runs
- 19 from a tubing hanger at the wellhead to an
- 20 injection packer set within the downhole liner at
- 21 a position below the production flow entry
- point(s) to the well, and of which tubing string
- the pump assembly is an element set at a depth
- 24 appropriate to reservoir performance
- 25 characteristics.
- 26 8. The method of any preceding claims whereby
- 27 hydrocarbons emanating from the production zone
- of the well and thus being present in the lower
- 29 annulus formed by the inner and outer tubing
- 30 strings enter the pump unit at the local pressure
- and pass through the impeller stages to be
- 32 discharged from the pump unit at an elevated

pressure into the upper annulus with the packoff 1 2 ensuring separation of the high and low pressure 3 fluids across the pump. 9. The apparatus of claim 2 wherein 4 the 5 assembly is provided as part of the outer tubing 6 string. 10. The apparatus of claims 2 and 9 wherein the lower 7 inner tubing string runs from the pump assembly 8 9 to the injection packer. 11. The apparatus of claims 2, 9 and 10 wherein the 10 upper inner tubing string is a separate item run 11 from the wellhead to the pump assembly subsequent 12 to the installation downhole of the outer tubing 13 14 string of claim 9. 15 16







Application No:

GB 0202823.1

Claims searched:

1-11

Examiner: Date of search: Dr. Lyndon Ellis

6 June 2002

Patents Act 1977 Search Report under Section 17

Databases searched:

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK Cl (Ed.T): ElF FLM, FMU

Int Cl (Ed.7): E21B

Online: EPODOC, WPI, JAPIO Other:

Documents considered to be relevant:

Category	Identity of document and relevant passage		
X, P	GB 2358202 A	(Mentor) Whole document, noting fig 2 and page 3, lines 21 to page 4, line 19	1 at least
x	GB 2324108 A	(Weir) Whole document	1-11
A	US 6056054	(Atlantic)	-

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